

CRF 2022 Rating Formulae		NOTE: CRF formulae, factors and ratings are subject to change each calendar year					
2/21/22							Notes
Base Rating	$R1 = 0.06 * (L * S) / (.75 * DSPS / 64)^{.33} + 0.3 * L + 0.20 * S + DC + LBRC + StabC$						1
Rated Length:	L=Base Sailing Length (L1) + a length increment (DeLL) for recent designs with broad sterns						
	L = L1 + DeLL						
	If LWL >= 0.65 * LOA,	L1 = 1.02 * (LOA + 4 * LWL) / 5					2
	If LWL < 0.65 * LOA,	L1 = 1.02 * (LOA + 4 * 0.65 * LOA) / 5					3
	If Age < 1990,	DeLL = 0					
	If Age => 1990 & Bm10 / Bmax <= 0.75:	DeLL = 0					4
	If Age => 1990 & Bm10 / Bmax > 0.75:	DeLL = L1 * [15 * {(Bm10 / Bmax) - 0.75} ^ 2.3]					
Rated S:	S=Sq Root of upwind + downwind sail areas, adjusted for rig and shroud types						5
	$S = \{Rig\ Type\ Factor * Shroud\ Type\ Factor * (RSAup + RSAdn) / 2\}^{.5}$						6
RSAup; Rated SA, Upwind;	RSAup = Jib + Main + Mizzen + Foresail						
	RSAup = RSAF + RSAM + RSAY + RSAG						
Rated Foretriangel Area, if LP% > 1;	If LP% > 1.0: RSAF = 0.55 * IG * J * {1 + 1.5 * ((LP% * J) - J) / (LP% * J)}						
Rated Foretriangel Area, if LP% <= 1;	If LP% <= 1.0: RSAF = 0.55 * .96 * (IG62 + j^2)^0.5 * J * LP%						
Rated Mainsail Area, for Jib Headed Main;	w/o main girths:	RSAM = .45 * P * E					
	w/main girths:	RSAM = (RSAM21 + RSAM22) / 2					
		RSAM21 = .45 * P * E					
		RSAM22 = .75 * (P/2 * (MGM + E) / 2 + P/4 * (MGM + MGU) / 2 + P/8 * (MGU + MGT) / 2 + P/8 * (MGT/2)					7
		MGM, MGU & MGT: declared mainsail girths required for all new mains					
Rated Mainsail Area for Gaff Headed Main;	If PG > 0:	RSAM = 0.55 * PG * E					
Rated Mizzen Area;	If PY > 0:	RSAY = 0.5 * PY * EY					
Rated Foresail Area, Schooner's;	If B1 > 0:	RSAG = 0.4 * (P1 + P3) / 2 * B1					
RSAdn; Rated SA, downwind;	RSAdn = Spin + Main + Mizzen + Foresail						
	RSAdn = SPIN + RSAM + RSAY + RSAG						
	If S-SPIN > A-SPIN: SPIN = S-SPIN						
	If S-SPIN <= A-SPIN: SPIN = A-SPIN						
	w/o declared SMW:	S-SPIN = 0.95 * (ISP^2 + J^2)^0.5 * 1.8 * SPL * 0.8 * 1.05					8
	w/declared SMW:	S-SPIN = (S-SPIN21 + S-PIN22) / 2					
		S-SPIN21 = 0.95 * (ISP^2 + J^2)^0.5 * 1.8 * SPL * 0.8 * 1.05					
	If SMW > 1.8 * SPL, S-SPIN22 =	S-SPIN21 * SMW / SPL					
	If SMW <= 1.8 * SPL, S-SPIN22 =	S-SPIN21					
		SMW = declared s-sail mid width required for all new s-sails					
	w/o declared AMG:	A-SPIN = 0.95 * (ISP^2 + TSP^2)^0.5 * 1.75 * TSP * 0.75 * 1.0					
	w/declared AMG:	A-SPIN = (A-SPIN21 + A-SPIN22) / 2					
	If AMG > 1.8 * TPS, A-SPIN22 =	A-SPIN21 * AMG / TPS					
	If AMG <= 1.8 * TPS, A-SPIN22 =	A-SPIN21					
		SMW = declared s-sail mid width required for all new s-sails					

	Displacement	DSPS	Declared value for boat weight as raced, without crew, in pounds	9
	Draft Correction	DC	Based on the difference between a Base Draft (BD) and the Rated Draft (RD)	10
			If RD>BD: $DC = 0.2 * L1 * ((RD/BD)^{1.5} - 1)$	
			If RD>BD: $DC = 0.2 * L1 * ((RD/BD)^{2.0} - 1)$	
			Base Draft: $BD = -0.0006 * L1^2 + 0.192 * L1 + 1.16$	11
			Rated Draft: If no centerboard: $RD = DM$	12
			If Brd down draft (DMcb) > fixed draft: $RD = DM + 0.70 * (DMcb - DM)$	13
	Length/Beam Ratio Corr.	LBRC	Based on the difference between a Base Length Beam Ratio and a Rated Length Beam Ratio	14
			$LBRC = 0.25 * L * ((RLBR / BLBR)^{0.20} - 1.0)$	
			Base LBR: $BLBR = 0.037 * L1 + 1.66$	15
			Rated LBR: $RLBR = L / Bmax$	
	Stability Correction	StabC	Based on the difference between a base righting moment and a calculated righting moment.	16
			Makes use of declared ballast weight, calculated hydrostatics, and a calculated default crew weight	
			If Rmtot > Rmbase: $StabC = 0.10 * L1 * ((Rmtot / Rmbase)^{2.0} - 1.0)$	17
			If Rmtot <= Rmbase: $StabC = 0.10 * L1 * ((Rmtot / Rmbase)^{0.2} - 1.0)$	18
			$Rmtot = RMhull + RMCrew$	19
			$RMhull = DSPS * GMT * 0.0175$	
			$GMT = It / (DSPS / 64) + VCB - VCG$	
			$It = BWL^3 * L * 0.034$	
			$BWL = Bmax^{.92} * (Dh * 7.25 / Bmax)^{0.08}$	
			$VCB = -1 * (((DSPS / 64 - Ballast / 690) * .35 * Dh) + (Ballast / 690 * (Dh + (DM - Dh) / 2))) / (DSPS / 64)$	
			$Dh = (DSPS / 64 - Ballast / 690) / (LWL * Bmax * 0.9 * Cp * Cms)$	
			Assumed canoe body Coefficient: $Cp = 0.55, Cms = .65$	
			$VCG = ((DSPS - Ballast) * CGnet + (Ballast * CGkeel)) / DSPS$	
			$CGnet = 0.60 * (L1 / Dh)^{0.5}$	20
			$CGkeel = -(Dh + (Dm - Dh) / 2) * (Keel Factor + 0.03)^{.3}$	
			If $Bm10 / Bmax > 0.75$: $Rmcrew = (CrewCt - 2) * 185 * ((Bm10 + Bmax) / 2 * 0.57 - 0.5 - 0.1 * Dh)$	21
			If $Bm10 / Bmax <= 0.75$: $Rmcrew = (CrewCt - 2) * 185 * (Bmax * 0.45 - 0.5 - 0.1 * Dh)$	
			$CrewCt = CrewWgt / 185$	22
			$CrewWgt = ((DSPS / 2240 / (0.01 * LWL)^3) / 254)^{0.375} * (RmHull / (DSPS * Bmax) / 0.006)^{0.4} * L1^{1.5} * 7.6$	23
			$RmBase = 24.2 * (BWL * L1^{0.25})^2 - 388 * (BWL * L1^{0.25}) + 2756$	24
			If $RmTot > RmBase$: $StabC = 0.10 * L1 * ((RmTot / RmBase)^{1.60} - 1)$	25
			If $RmTot <= RmBase$: $StabC = 0.10 * L1 * ((RmTot / RmBase)^{0.20} - 1)$	
CRF 2022 Rating	Rating		$R(ft) = R1 * Prop * DLF * SaDF * Keel * Spar * MAF$	26
			$R(sec/mi) = 0.6 * 3600 * \{1 / (Rft)^{0.5} - 1 / (100)^{0.5}\} - 90$	27
			$R(GPH) = R(sec/mi) + 535$	28
Prop Factor (Prop)	Prop		Prop = assigned prop factor, based on installation type	29
Disp/Length Factor	DLF		Based on the difference between a base Disp/Length ratio and the actual Disp/Length ratio	
			If $DLFbase > 1.015$: $DLF = DLFbase + (1 + DLFbase - 1.015)^{4.0} - 1$	30
			If $DLFbase <= 1.015$: $DLF = DLFbase + (1 + DLFbase - 1.015)^{0.5} - 1$	
			Base $DLF = ((350 - 2.9 * L) / ((Disp / 2240) / (0.01 * L)^3))^{0.025}$	31
Sail Area/Disp Factor	SaDF		Based on the difference between a base SA/Disp ratio and the actual SA/Disp ratio	
			If $SaDFbase > 1.0130$: $SaDF = Base SaDF + (1 + SaDFbase - 1.013)^{5.0} - 1$	32
			If $SaDFbase <= 1.0130$: $SaDF = SaDFbase$	
			Base $SaDF = ((S^2 / (DSPS / 64)^{0.67}) / (0.18 * L1 + 19.5))^{0.040}$	33
Keel Type Factor	Keel		Keel = Assigned Keel Factor, based on keel type	34
Spar Material Factor	Spar		Spar = Assigned Spar Factor, based on spar construction material	35
Moveable Appendage Factor	MAF		MAF = Moveable Appendage Factor (for a keel Trim Tab, if fitted)	36

	<u>Notes</u>	<u>Comments</u>	
1		The basic architecture of the 2017 reformulation of CRF was adapted from Nat Herreshoff's Universal Rule and from Olin Stephens' (et al) International Offshore Rule . Despite shortcomings exposed by aggressive exploitation of loopholes over time, early versions of IOR did a quite good job of handicapping a variety boat boat sizes and types until it fell out of favor due to the humps, bumps and hollows that came to plague it in later years.	
2		Effective sailing length 'L' is a primary driver of performance, and is taken as a weighted average of LOA and LWL, with LWL recognized as having a stronger effect on performance potential than LOA.	
3		A cap on total overhang of 35% of LOA (typical of International Rule boats) limits any rating advantage stemming from extreme overhang lengths and/or profile slopes (eg Sonder and Square Meter classes)	
4		A declaration for Bm10 is only required for design dates after 1990. It addresses the added effective sailing length resulting from broad, powerful sterns in some contemporary designs.	
5		The square root of sail area is taken to keep the rated units uniform in linear feet. For non-spinnaker ratings, $RSAdn = RSAup$	
6		See table of assigned Rig and Shroud Type factors	
7		CRF 2022 addresses mainsail roach profiles that vary from the $.22 * E$ (MGT), $.38 * E$ (MGU) and $.65 * E$ (MGM) that were previously taken as defaults. Starting with CRF 2022, calculations for RSAM depend on actual measured MGT, MGU and MGM, that are required declarations for newly built mainsails only. Mainsails whose roach is larger than the previous default will now rate slightly faster, and roaches that are smaller will rate slightly slower.	
8		CRF 2022 addresses spinnaker mid widths that are greater than $1.8 * SPL$ (s-sails) or $1.8 * TPS$ (a-sails). Starting with CRF 2022, calculations for S-SPIN depend on actual measured SMW and/or AMG, that are required declarations for newly built spinnakers. Spinnakers whose mid widths are larger than $1.8 * SPL$ (s-sails) or $1.8 * TPS$ (a-sails) will rate slightly faster. Spinnakers whose mid widths are smaller than the default will not rate slower, to discourage attempts at rating optimization via small spinnaker area.	

9	The declared DSPS is to be the estimated weight of the yacht as presented for racing, in pounds, excluding crew weight. For yachts that are primarily raced and daysailed, this is similar to 'light ship' (empty tanks, with minimal food and gear). For yachts that are equipped and provisioned for cruising while racing, this is similar to 'half load' (tanks half full, with ordinary food and gear) .	
10	Rated Draft (RD) deeper than Base Draft (BD) speeds up rating	
11	Base Draft (BD) is based on a second order polynomial fit to draft vs length across the Classic fleet	
12	DM=maximum fixed draft.	
13	DMcb=max centerboard down draft. CRF 2021 rates centerboard boats for 70% of the added depth of the board extension below the fixed draft	
14	Length/beam ratio higher than base (for a long, narrow hull) speeds up rating	
15	Base Length/Beam Ratio (BLBR) is based on a second order polynomial fit to LOA/Bmax ratios across the Classic fleet	
16	Stability is a primary driver of sailboat performance potential, but physically measuring it is not a reasonable or practical logistical and cost hurdle to impose on the Classic fleet. Short of actual stability measurement, the next best thing is to influence ratings via stability that is calculated rather than measured. Higher calculated stability does result in a faster CRF rating, but the effect is kept modest due to the limited input data.	
17	Calculated stability (RmTot) that is higher than base stability (RmBase) speeds up rating	
18	If ballast weight is uncertain or unknown, a value is assigned that is typically 0.4*DSPS	
19	RmTot = Calculated stability including effect of crew weight	
20	VCG of net construction weight (DSPS - Ballast). Empirically derived	
21	The crew moment arm for contemporary boats with broad beam aft is greater than it is for typical Classic hulls.	

22	Crew count assumes an average crew weight of 185 pounds.	
23	Calculated crew weight taken from a recognized IMS formulation	
24	Base RM includes crew weight, and is based on a second order polynomial fit to Rmtot vs a function of Bmax and L across the Classic fleet	
25	High stability (RMTot >RMBase) speeds up rating	
26	The rating in decimal feet reflects speed potential as implied by the square root of an effective sailing Length.	
27	Sec/mi, normalized to typical PHRF handicaps w/scratch R=100	
28	Sec/mi, normalized to VPP GPH ratings, eg via ORCi or ORR	
29	See table of assigned factors	
30	A Disp/length ratio lower than base (long, light boat) speeds up rating	
31	The Base DLF is a linear function that reflects the Disp/L distribution across the Classic fleet	
32	A SA/Disp ratio higher than base (high power to weight ratio) speeds up rating	
33	The Base SaDF is a linear function that reflects the SA/Disp distributioin across the Classic fleet	
34	See table of assigned keel typefactors. The factors used reflect the differences in appendage wetted area and aspect ratio, rudder efficiency, VCB and VCG associated with the various keel types.	
35	See table of assigned spar material factors. The factors used reflect differences in stability and pitch moment of inertia associated with the different mast material types and number of masts.	
36	The MAF addresses the advantages of a keel trim tab, and is taken from IOR.	